

A Model Predictive Method for Specific Harmonic Reduction at Low Switching Frequency in Permanent Magnet Synchronous Motor

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Background - PMSM

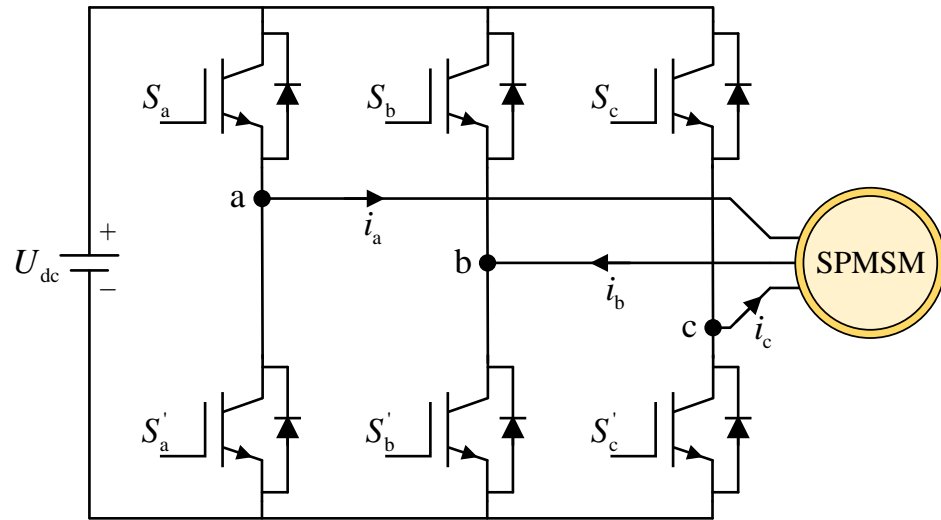


Fig. 1. Main circuit of PMSM drive system.

➤ Advantages of PMSM:

- ✓ Many industrial production applications.
- ✓ Higher power density.
- ✓ Lower operating cost.



Fig. 2. 10,400kW “GuoNeng”, PMSM direct drive heavy duty electric locomotive

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Fig. 3. B2 Platform Train, Changsha Metro Line 5, using PMSM traction system

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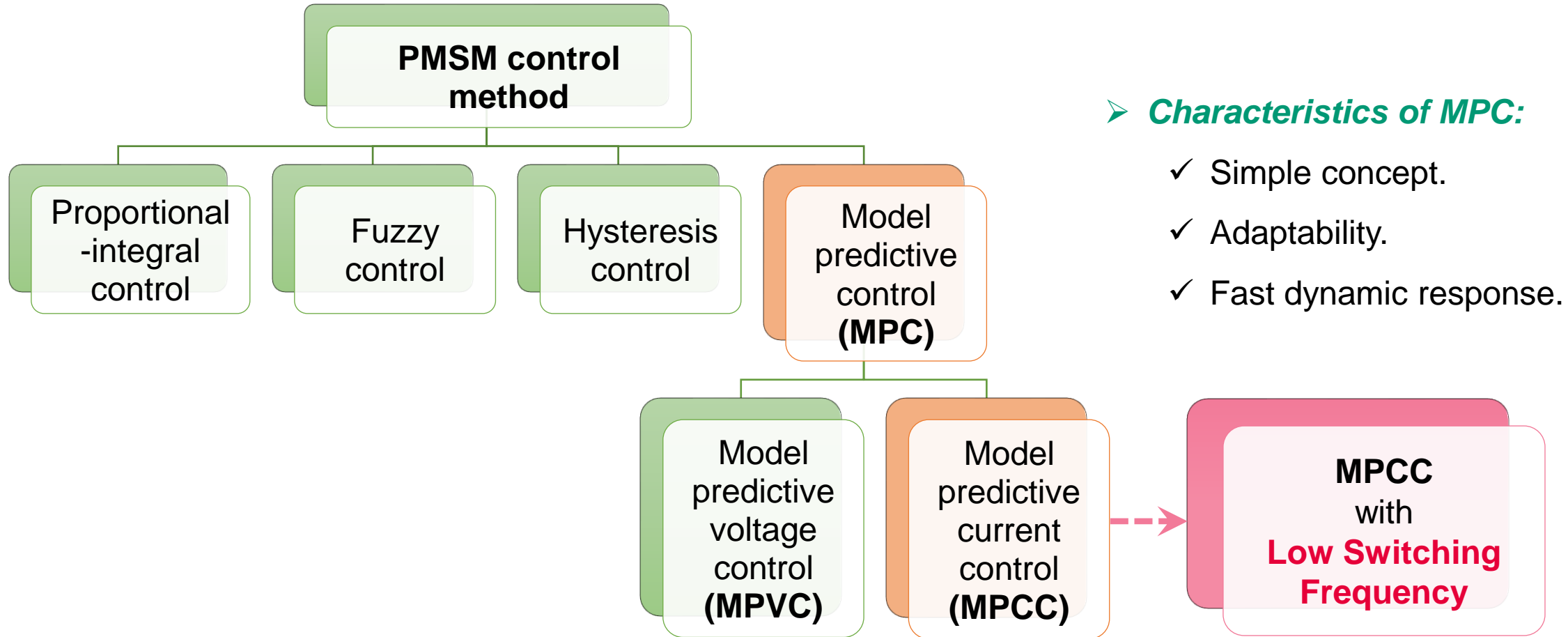


Fig. 2. PMSM control method

$$\begin{cases} u_d = Ri_d + L \frac{di_d}{dt} - \omega_e Li_q \\ u_q = Ri_q + L \frac{di_q}{dt} + \omega_e Li_d + \omega_e \psi_f \end{cases}$$

Traditional PMSM model

➤ **Shortcomings in T-LSF-MPCC method:**

- Frequency reduction limit only.
- Make more lower (5th, 7th etc.) harmonics*.
- Harmonic parts are not included in the model.
- Harmonic current prediction is not possible.

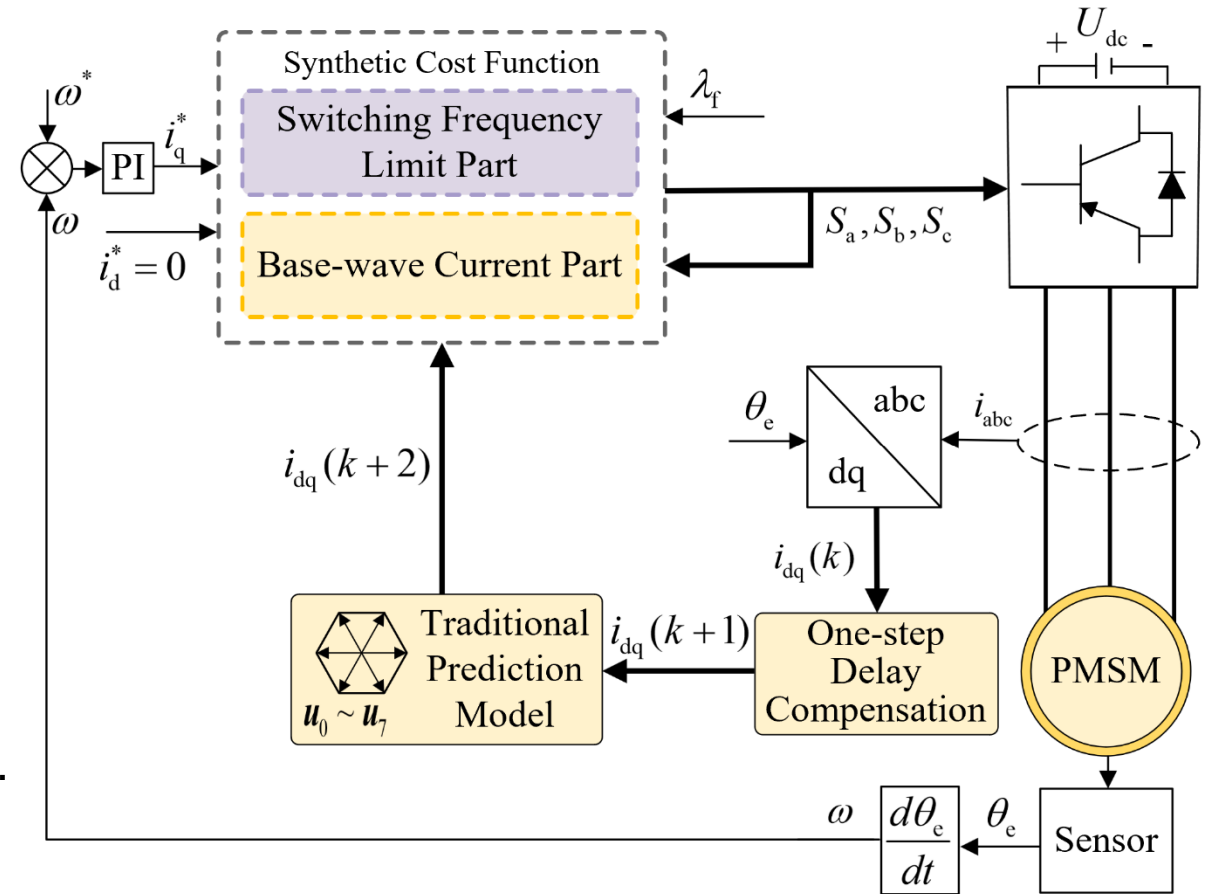


Fig. 4. Block diagram of T-LSF-MPCC Method

* Z. Chen et.al, "Evaluation of the Harmonics in PMSM with Low Switching Frequency Power Supply"

- *To address the shortcomings of T-LSF-MPCC, the problems that should be solved in this study are as follows:*



- 1. Organize the PMSM model containing harmonic currents.
- 2. Extract harmonic currents.
- 3. Combined model current prediction.
- 4. Integration with "low switching frequency".

Model Predictive Specific Harmonic Reduction Control (MPSHRC)

is proposed

Method - Overview

➤ **Core parts of MPSHRC method:**

- 1. Harmonic Current Extractor;
- 2. Harmonic Current Prediction;
- 3. Synthetic Cost Function.

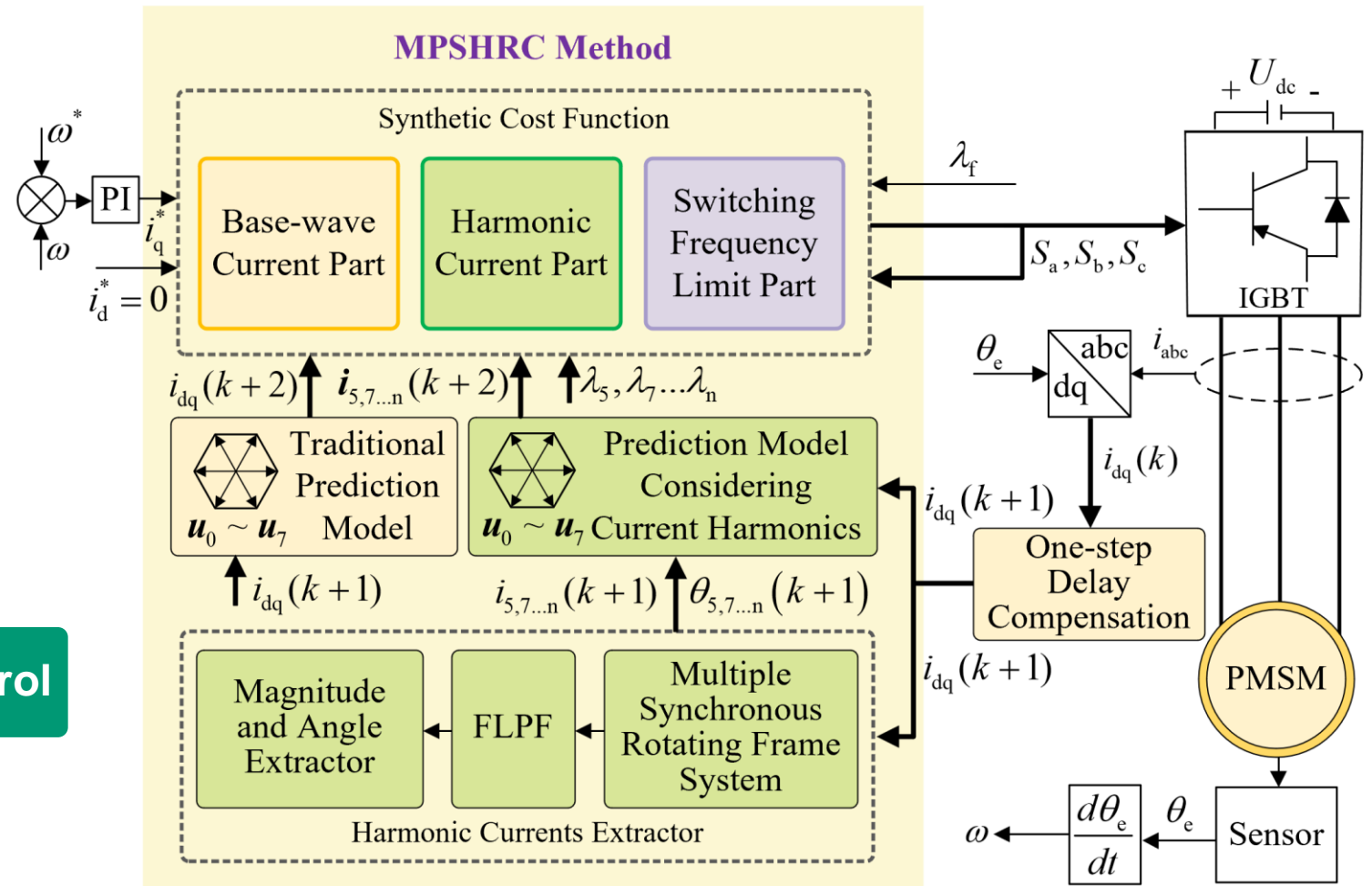


Fig. 5. Block diagram of proposed MPSHRC Method

1. Harmonic Current Extractor

➤ 1.1 PMSM Current Equation Considering Harmonics

$$\begin{cases} i_d = i'_d + \sum_{n=6k\pm 1, k\geq 1}^{k\rightarrow\infty} i_d^n \\ i_q = i'_q + \sum_{n=6k\pm 1, k\geq 1}^{k\rightarrow\infty} i_q^n \end{cases}$$

Forms of value and phase angle :

$$\begin{cases} i_d = i_1 \cos \theta_1 + \sum_{n=6k\pm 1, k\geq 1}^{k\rightarrow\infty} i_n \cos (6k\omega_e t + \theta_n) \\ i_q = i_1 \sin \theta_1 + \sum_{n=6k\pm 1, k\geq 1}^{k\rightarrow\infty} i_n \sin (6k\omega_e t + \theta_n) \end{cases}$$

Rotation speed

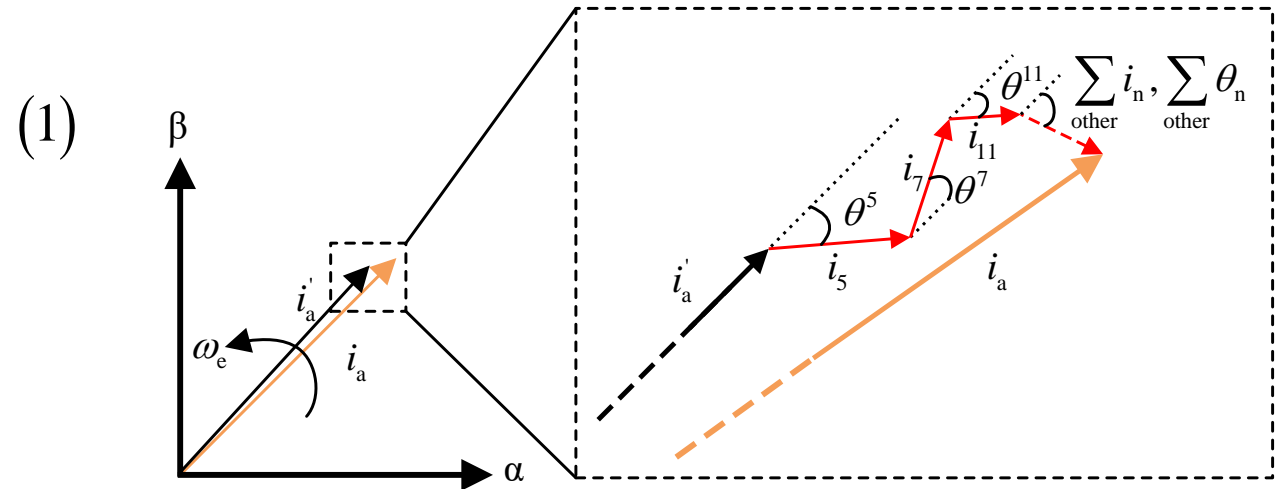


Fig. 6. PMSM stator current with all $6k \pm 1$ current harmonics in the $\alpha\beta$ axes.

(2)

1. Harmonic Current Extractor

➤ 1.1 PMSM Current Equation Considering Harmonics

$$\begin{cases} i_d = i'_d + i_d^5 + i_d^7 = i_1 \cos \theta_1 + i_5 \cos(6\omega_e t + \theta_5) + i_7 \cos(6\omega_e t + \theta_7) \\ i_q = i'_q + i_q^5 + i_q^7 = i_1 \sin \theta_1 + i_5 \sin(6\omega_e t + \theta_5) + i_7 \sin(6\omega_e t + \theta_7) \end{cases} \quad (3)$$

$$\begin{cases} u_d = Ri_d + L \frac{di_d}{dt} - \omega_e Li_q \\ u_q = Ri_q + L \frac{di_q}{dt} + \omega_e Li_d + \omega_e \psi_f \end{cases} \quad (4)$$

$$\begin{cases} u_d = R(i'_d + i_d^5 + i_d^7) + L \left(\frac{d}{dt} (i'_d + i_d^5 + i_d^7) - \omega_e (i'_q + i_q^5 + i_q^7) \right) \\ u_q = R(i'_q + i_q^5 + i_q^7) + L \left(\frac{d}{dt} (i'_q + i_q^5 + i_q^7) + \omega_e (i'_d + i_d^5 + i_d^7) \right) + \omega_e \psi_f \end{cases} \quad (5)$$

Voltage equation for dq-axes considering harmonic currents, Will be used in the method analysis

1. Harmonic Current Extractor

➤ 1.2 Multiple Synchronous Rotating Frame System

$$\begin{bmatrix} i_d^{5F} \\ i_q^{5F} \\ i_d^{7F} \\ i_q^{7F} \end{bmatrix} = \begin{bmatrix} \cos(5\omega_e t) & -\sin(5\omega_e t) \\ \sin(5\omega_e t) & \cos(5\omega_e t) \\ \cos(7\omega_e t) & \sin(7\omega_e t) \\ -\sin(7\omega_e t) & \cos(7\omega_e t) \end{bmatrix} \begin{bmatrix} i_\alpha \\ i_\beta \end{bmatrix} \quad (6)$$

Note: Only the fundamental frequency axes and the 5th and 7th order axes are listed.

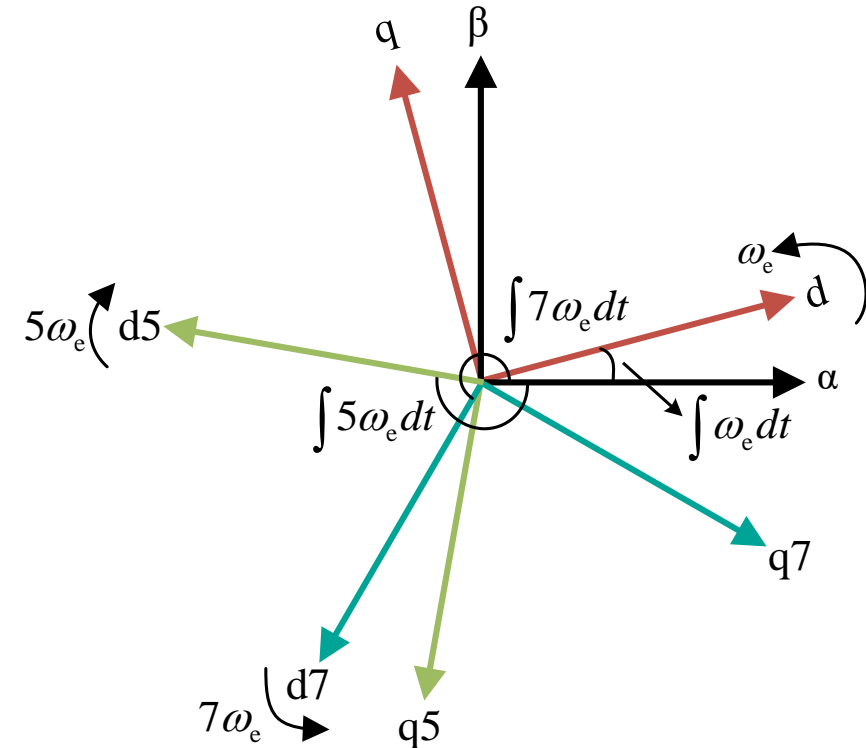


Fig. 7. MSRFS Method.

1. Harmonic Current Extractor

➤ 1.3 Calculation of Harmonic Currents in Each dq axes

Harmonic current extraction using first-order low-pass filter (FLPF). The input-output relation equation of the FLPF after back-ward Eulerian discretization is

$$y(k) = \frac{2\pi f_n T_s}{1 + 2\pi f_n T_s} x(k) + \frac{1}{1 + 2\pi f_n T_s} y(k-1) \quad (7)$$

The cutoff frequency is set to run at **10 Hz**, which is much lower than the 6th harmonic frequency in synchronous rotating coordinate system.

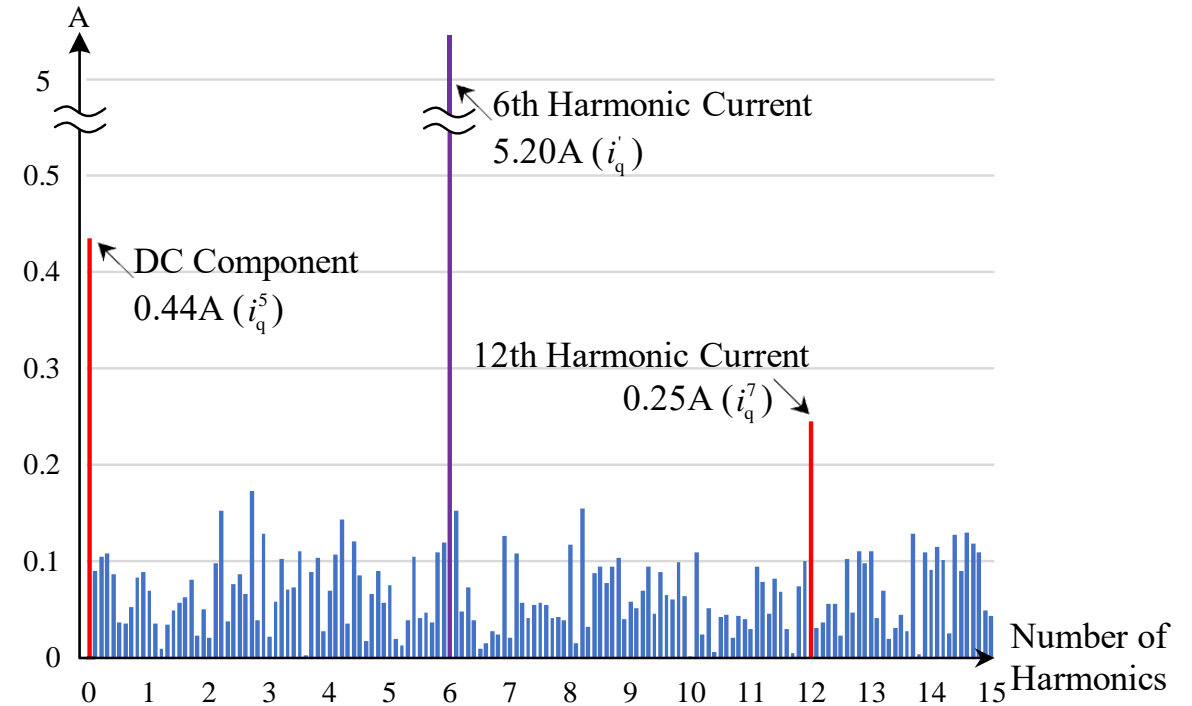


Fig. 8. FFT analysis of i_q^{5F} .

1. Harmonic Current Extractor

➤ 1.3 Calculation of Harmonic Currents in Each dq axes

Vectors synthesized from 5th,7th dq axes harmonic currents can be calculated by

$$\begin{cases}
 i_5 = \sqrt{(i_d^5)^2 + (i_q^5)^2}, i_7 = \sqrt{(i_d^7)^2 + (i_q^7)^2} \\
 \theta_5 = \arctan \frac{i_q^5}{i_d^5}, \theta_7 = \arctan \frac{i_q^7}{i_d^7} \\
 i_5 = i_5 e^{j\theta_5}, i_7 = i_7 e^{j\theta_7}
 \end{cases} \quad (8)$$

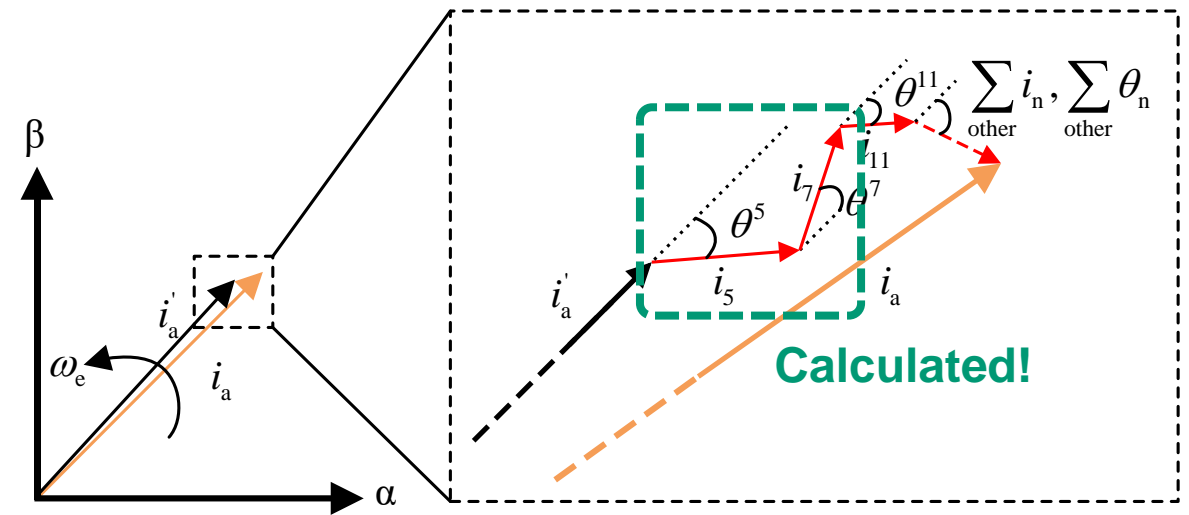


Fig. 6. PMSM stator current with all $6k \pm 1$ current harmonics in the $\alpha\beta$ axes.

Next step: current prediction

2. Harmonic Current Prediction

➤ 2.1 Prediction Model Considering Current Harmonics

Starting with traditional model...

$$\begin{cases} u_d = Ri_d + L \frac{di_d}{dt} - \omega_e Li_q \\ u_q = Ri_q + L \frac{di_q}{dt} + \omega_e Li_d + \omega_e \psi_f \end{cases} \quad (9) \xrightarrow[\text{One-step delay}]{\text{Euler forward}} \begin{cases} i_d^p(k+1) = (1 - \frac{T_s R}{L})i_d(k) + \frac{T_s}{L}u_d(k) + T_s \omega_e i_q(k) \\ i_q^p(k+1) = (1 - \frac{T_s R}{L})i_q(k) + \frac{T_s}{L}u_q(k) - T_s \omega_e i_d(k) - \frac{T_s \omega_e \psi_f}{L} \end{cases} \quad (10)$$

$$\begin{cases} i_d^p(k+2) = (1 - \frac{T_s R}{L})i_d(k+1) + \frac{T_s}{L}u_d(k) + T_s \omega_e i_q(k+1) \\ i_q^p(k+2) = (1 - \frac{T_s R}{L})i_q(k+1) + \frac{T_s}{L}u_q(k) - T_s \omega_e i_d(k+1) - \frac{T_s \omega_e \psi_f}{L} \end{cases} \quad (11)$$

Euler forward Prediction

Substitute into

$$\begin{cases} i_d = i'_d + i_d^5 + i_d^7 \\ i_q = i'_q + i_q^5 + i_q^7 \end{cases} \quad (3)$$

Proposed harmonic current equation

2. Harmonic Current Prediction

➤ 2.1 Prediction Model Considering Current Harmonics

$$\left\{ \begin{array}{l} i_d^{5p}(k+2) = i_d^{5p}(k+1) - T_s \left(\frac{d(i_d^{5p} + i_d^{7p})}{dt} \right) + T_s \left(\frac{u_d - Ri_d^p(k+1) + \omega_e Li_q^p(k+1)}{L} \right) \\ i_q^{5p}(k+2) = i_q^{5p}(k+1) - T_s \left(\frac{d(i_q^{5p} + i_q^{7p})}{dt} \right) + T_s \left(\frac{u_d - Ri_q^p(k+1) - \omega_e (Li_d^p(k+1) + \psi_f)}{L} \right) \\ i_d^{7p}(k+2) = i_d^{7p}(k+1) - T_s \left(\frac{d(i_d^{5p} + i_d^{7p})}{dt} \right) + T_s \left(\frac{u_d - Ri_d^p(k+1) + \omega_e Li_q^p(k+1)}{L} \right) \\ i_q^{7p}(k+2) = i_q^{7p}(k+1) - T_s \left(\frac{d(i_q^{5p} + i_q^{7p})}{dt} \right) + T_s \left(\frac{u_d - Ri_q^p(k+1) - \omega_e (Li_d^p(k+1) + \psi_f)}{L} \right) \end{array} \right. \quad (12)$$

Need to define the derivative term

2. Harmonic Current Prediction

➤ 2.1 Prediction Model Considering Current Harmonics

The derivative of each harmonic is defined as the value of the harmonic current derivative at the previous moment, which can be expressed as

$$\left\{ \begin{array}{l} \frac{di_d^p}{dt} = \frac{i_d^p(k+1) - i_d^p(k)}{T_s}, \frac{di_q^p}{dt} = \frac{i_q^p(k+1) - i_q^p(k)}{T_s} \\ \frac{di_d^{5p}}{dt} = \frac{i_d^{5p}(k+1) - i_d^{5p}(k)}{T_s}, \frac{di_q^{5p}}{dt} = \frac{i_q^{5p}(k+1) - i_q^{5p}(k)}{T_s} \\ \frac{di_d^{7p}}{dt} = \frac{i_d^{7p}(k+1) - i_d^{7p}(k)}{T_s}, \frac{di_q^{7p}}{dt} = \frac{i_q^{7p}(k+1) - i_q^{7p}(k)}{T_s} \end{array} \right. \quad (13)$$

It should be noted that the above equations is not limited to the 5th ,7th harmonics and can be further expanded.

2. Harmonic Current Prediction

➤ 2.2 Traditional Prediction Model

$$\begin{cases} i_d^p(k+2) = (1 - \frac{T_s R}{L})i_d(k+1) + \frac{T_s}{L}u_d(k) + T_s \omega_e i_q(k+1) \\ i_q^p(k+2) = (1 - \frac{T_s R}{L})i_q(k+1) + \frac{T_s}{L}u_q(k) - T_s \omega_e i_d(k+1) - \frac{T_s \omega_e \psi_f}{L} \end{cases}$$

Reasons for using **both models together**?

- Given quantities i_{dq}^* have dynamic characteristic;
- If only a harmonic model is used, the given quantities also need to be extracted harmonically;
- Will result in reduced dynamic effect and increased computational effort.

Next step: Synthetic Cost Function

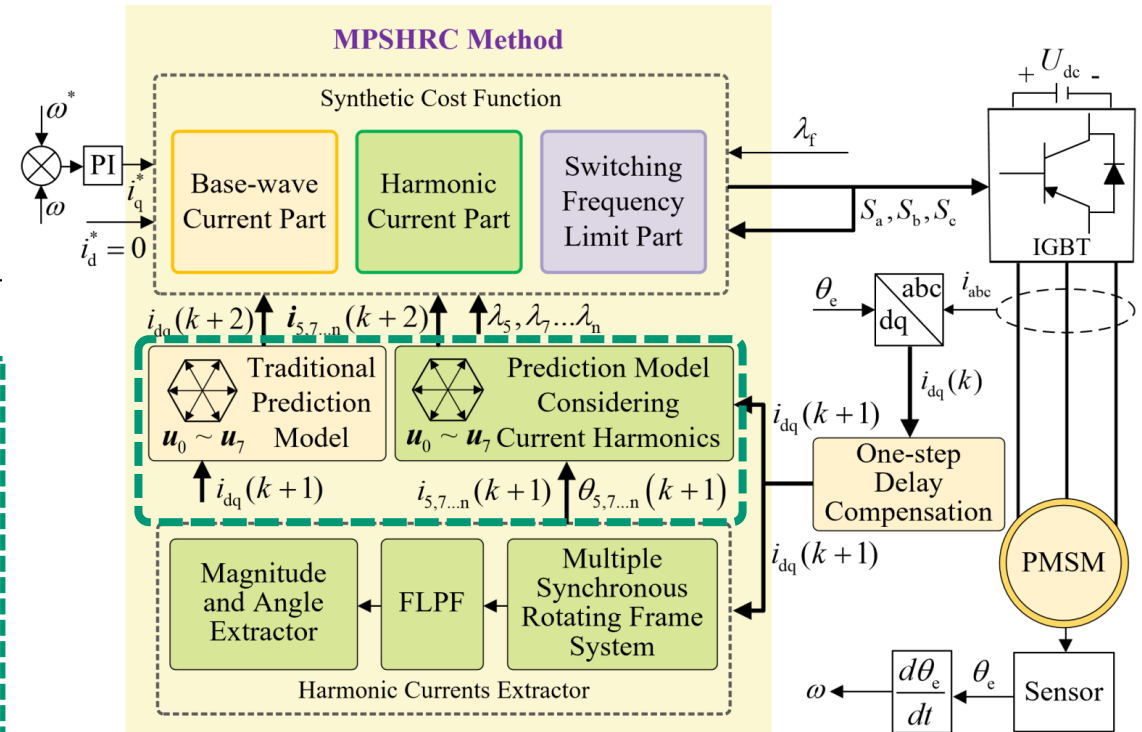


Fig. 5. Block diagram of proposed MPSHRC Method

3. Synthetic Cost Function

$$\begin{cases}
 J = g_b + g_h + g_s \\
 g_b = \left[i_d^* - i_d^p(k+2) \right]^2 + \left[i_q^* - i_q^p(k+2) \right]^2 \\
 g_h = \lambda_5 \left(\left(i_d^5(k+1) \right)^2 + \left(i_q^5(k+1) \right)^2 \right) \\
 \quad + \lambda_7 \left(\left(i_d^7(k+1) \right)^2 + \left(i_q^7(k+1) \right)^2 \right) \\
 g_s = \lambda_f \sum_{i=a,b,c} |S_i(k) - S_i(k-1)|
 \end{cases} \quad (14)$$

Selection of weighting factors:

- Calculation and analysis first;
- Further changing based on real results.

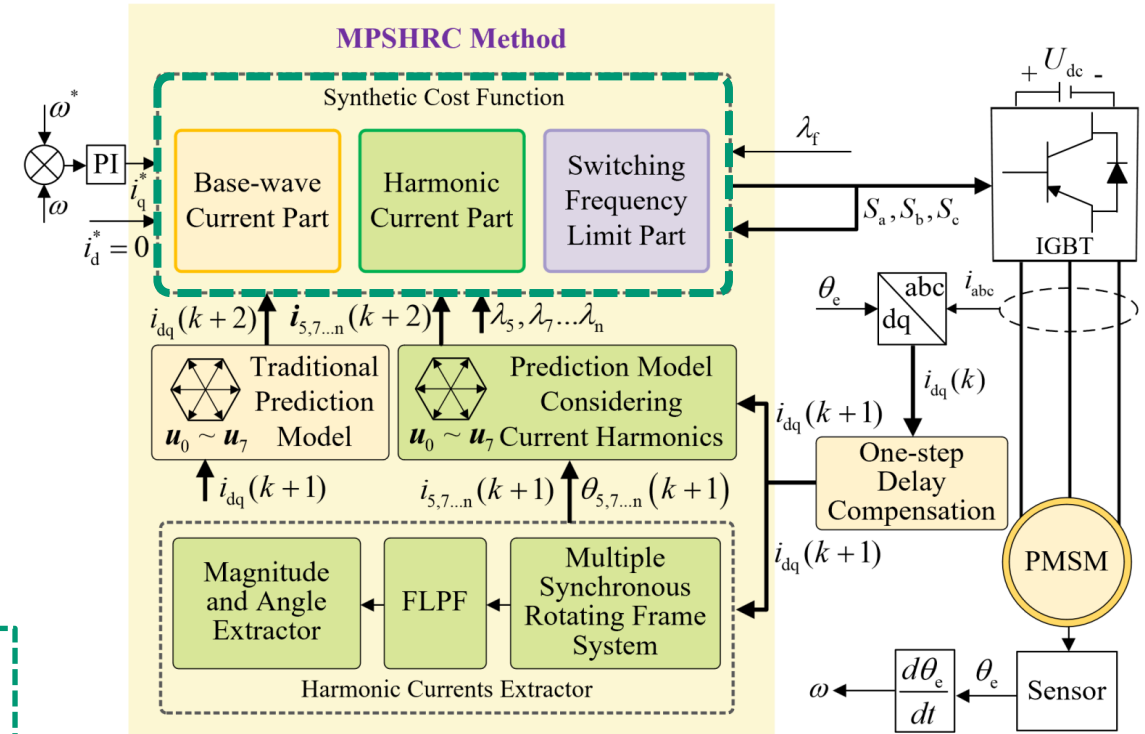
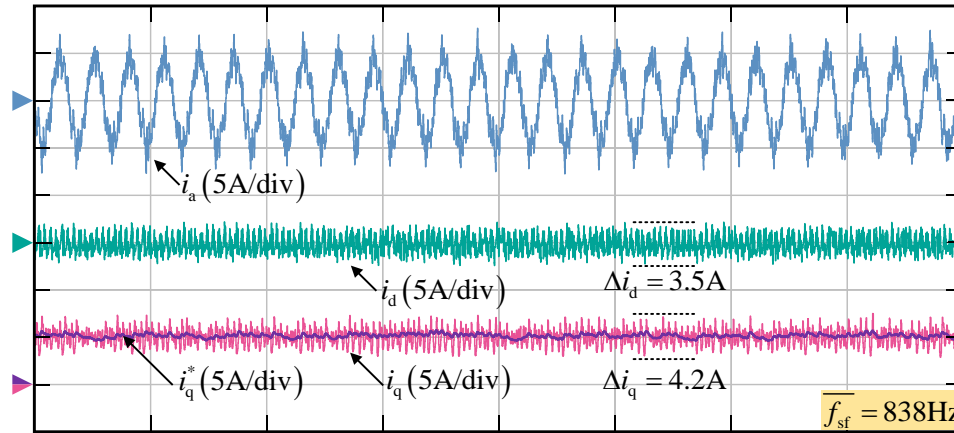


Fig. 5. Block diagram of proposed MPSHRC Method

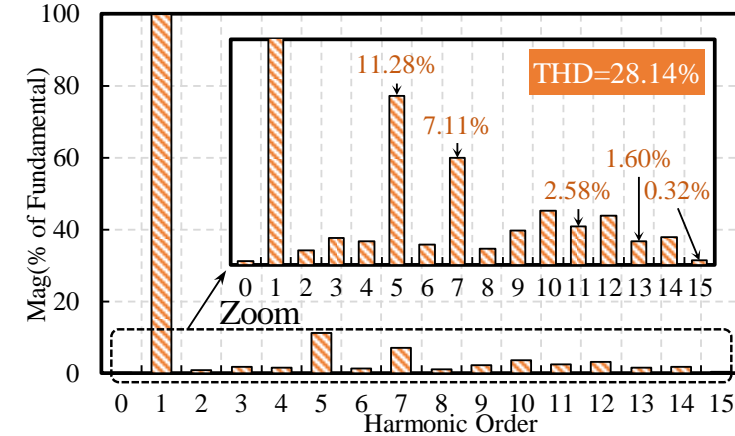
Results – High speed

The average switching frequency \bar{f}_L is **830Hz**.

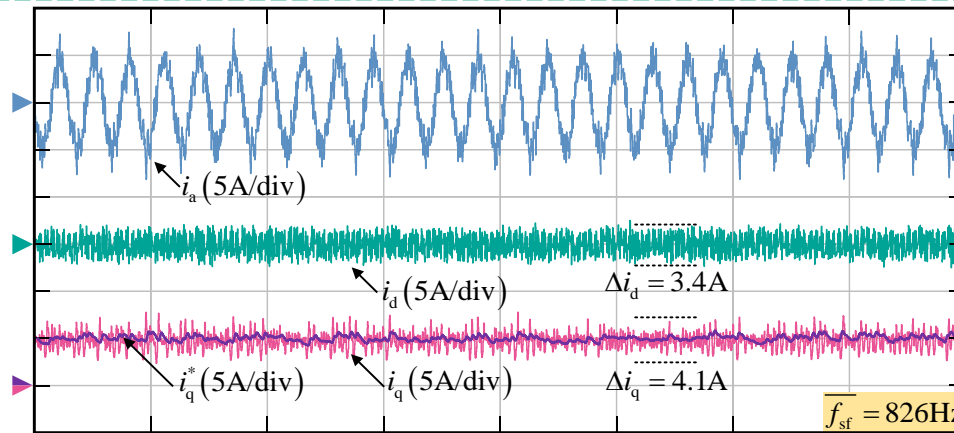
T-LSF-
MPCC
method



THD
Analysis
→
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current



Proposed
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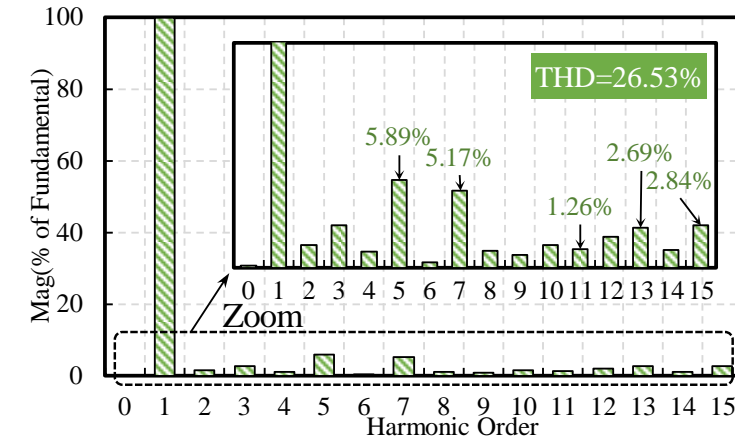
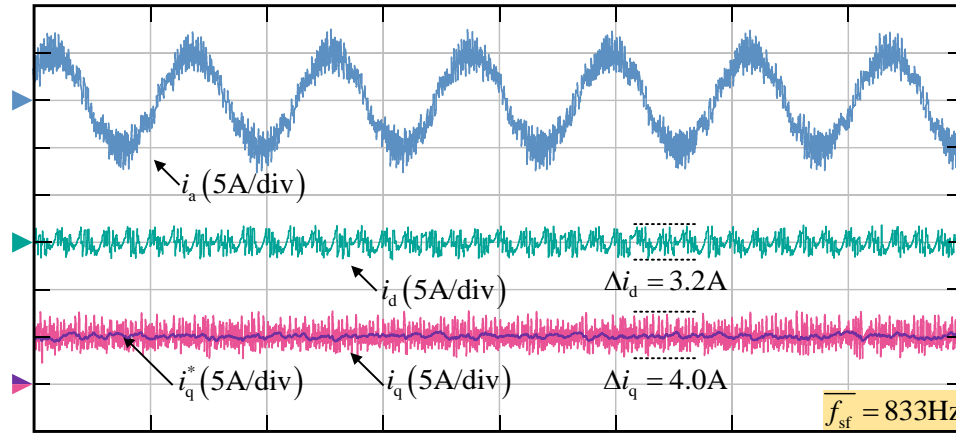


Fig. 9. Simulation results at rated torque (5N.m) and **rated speed(2000rad/min)**

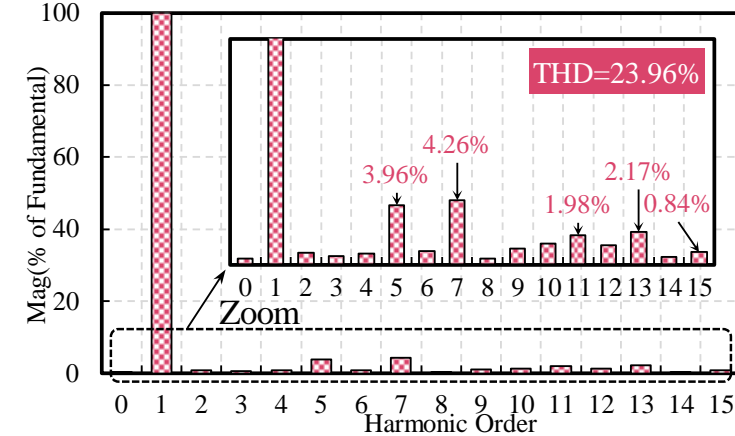
Results – Low speed

The average switching frequency \bar{f}_L is **830Hz**.

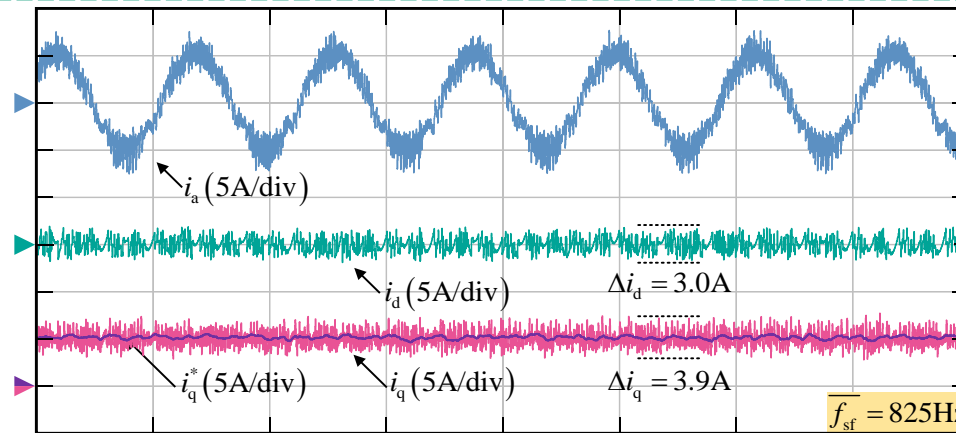
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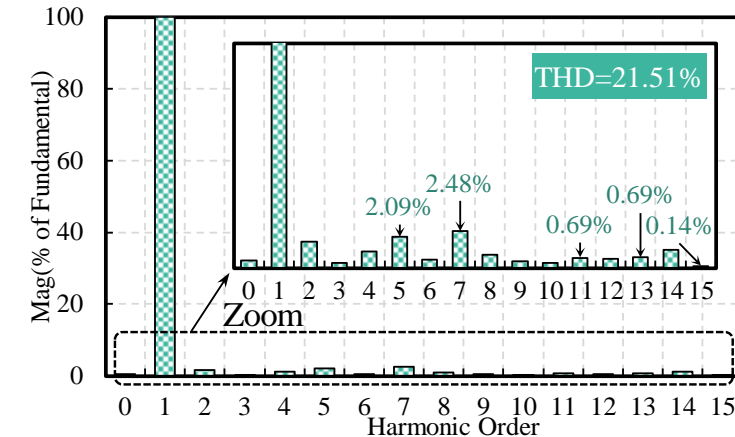


Fig. 10. Simulation results at rated torque (5N.m) and low speed(500rad/min)

- Considering the impact of low harmonics on PMSMs operating at low switching frequencies, This paper proposes a specific number of harmonics reduction method based on model predictive control.
- The method extracts the corresponding harmonics using **MSRFS** and uses the **next moment harmonic quantities predicted** by a mathematical model of the PMSM considering the harmonics, and **a synthetic cost function** is designed to optimize the system in conjunction with a finite-set model predictive control.
- Both demonstration and simulation validate the effectiveness of the proposed methodology and detailed data indications are given.

Thanks for your listening!

A Model Predictive Method for Specific Harmonic Reduction at Low Switching Frequency in Permanent Magnet Synchronous Motor

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